

# Stormwater Management

# Report

under the Town of Newbury Stormwater Management and Illicit Discharge and Erosion Control Bylaw

Fields Way 4-Lot Residential Subdivision

Assessor's Map R-20, Parcel 43A

170 Orchard Street Newbury, MA

January 4, 2023

# Applicant:

Estate of Lewis Bulgaris

# Submitted to:

Town of Newbury Planning Board



Prepared by: Griffin Engineering (

Griffin Engineering Group, LLC Beverly, MA

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## STORMWATER MANAGEMENT CHECKLIST



## Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

## **B. Stormwater Checklist and Certification**

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

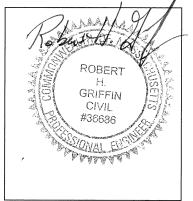
*Note:* Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

## **Registered Professional Engineer's Certification**

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



1/ 10/3/23

Signature and Date

#### Checklist

**Project Type:** Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



**LID Measures:** Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

- No disturbance to any Wetland Resource Areas
- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
  - Credit 1
  - Credit 2
  - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe):

#### **Standard 1: No New Untreated Discharges**

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



#### Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

#### Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

Static	Simple Dynamic
--------	----------------

Dynamic Field<sup>1</sup>

- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum
extent practicable for the following reason:

- Site is comprised solely of C and D soils and/or bedrock at the land surface
- M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
- Solid Waste Landfill pursuant to 310 CMR 19.000
- Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.

	Property inclu	des a M.G.L.	c. 21E site or a	solid waste la	andfill and a r	mounding anal	ysis is included.
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<sup>&</sup>lt;sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



#### Standard 3: Recharge (continued)

The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.

Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

#### **Standard 4: Water Quality**

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
  - is within the Zone II or Interim Wellhead Protection Area
  - is near or to other critical areas
  - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
  - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



## Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

Standard 4: Water Quality (continued)
$\boxtimes$ The BMP is sized (and calculations provided) based on:
The ½" or 1" Water Quality Volume or
The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
☐ The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
<ul> <li>The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.</li> <li>The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior to</i> the discharge of stormwater to the post-construction stormwater BMPs.</li> </ul>
☐ The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
All exposure has been eliminated.
All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Standard 6: Critical Areas
The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
Critical areas and BMPs are identified in the Stormwater Report.



# Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

- Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
- Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

#### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



# Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

#### **Standard 9: Operation and Maintenance Plan**

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
  - Name of the stormwater management system owners;
  - Party responsible for operation and maintenance;
  - Schedule for implementation of routine and non-routine maintenance tasks;
  - Plan showing the location of all stormwater BMPs maintenance access areas;
  - Description and delineation of public safety features;
  - Estimated operation and maintenance budget; and
  - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
  - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
  - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

#### Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

# ATTACHMENT A

PROJECT DESCRIPTION

## 1.0 INTRODUCTION

This stormwater management report was prepared in support of the proposed residential development at 170 Orchard Street (Assessors Map R-20 Lot 43A) in Newbury, MA. The project consists of constructing 500-ft of new road with four (4) new single-family lots.

According to the Massachusetts Department of Environmental Protection (MassDEP) Stormwater Management regulations, the proposed construction is exempt from MassDEP Stormwater Management requirements since the proposed development is a small residential subdivision (four or fewer lots). However, the regulations establish a framework for evaluating stormwater management systems that is used by the Town of Newbury in evaluating new development projects. The narrative below compares the proposed construction to the MassDEP Stormwater Management requirements.

#### 1.1 Existing Conditions

The project site is located at 170 Orchard Street (Map R-20, Lot 43A), in Newbury, Massachusetts. The 20.57-acre property is currently vacant, consisting primarily of agricultural fields and woods. A Bordering Vegetated Wetland (BVW) exists on the south-westerly side of the property, fed by a perennial stream. The property is surrounded by residential properties. Orchard Street is to the south. The site generally slopes west-southwest toward the BVW.

#### 1.2 Proposed Conditions

The project involves constructing a new 500-ft long roadway to serve four new singlefamily residences with associated driveways, utilities, septic systems, stormwater management features, and landscaping. A site plan showing the proposed development and stormwater management features is separately provided.

The project is considered new development under the Stormwater Management regulations. When complete, the project will have created approximately 41,950 square feet of impervious surfaces at the site, consisting of the roadway, driveways, and four residences.

## 2.0 STORMWATER MANAGEMENT STANDARDS

#### 2.1 Standard 1: No New Untreated Discharges

No new untreated discharges to wetlands or waterways proposed.

#### 2.2 Standard 2: Peak Rate Attenuation

Hydrologic modeling was conducted using the HydroCAD computer model. This model uses an approximation of Soil Conservation Service TR-20 methods to calculate runoff rates and volumes based on descriptions of land use, ground characteristics, and size.

The time of concentration (Tc) for each subcatchment was calculated in HydroCAD using a combination of sheet flow and shallow concentrated flow. Sheet flow uses roughness coefficients (Manning's n) and watercourse slope to calculate travel time of stormwater runoff for each subcatchment. Per Town of Newbury regulations, the site was modeled using a maximum of 50-feet of sheet flow. The shallow concentrated flow method was used to determine the velocity factor along the flow path of the runoff and thereby derive a travel time. The time of concentration of each subcatchment is the combination of these travel times. A minimum time of concentration of 6 minutes was used for all subcatchments, for both existing and proposed conditions.

The enclosed drainage calculations indicate a decrease in the post-development peak runoff rates for the 2-, 10-, and 100-year, 24-hour storm events from the site (the HydroCAD drainage calculations for the aforementioned storm events are provided in Attachment F). The design storms were based on rainfall intensities recommended by the Cornell University Regional Climate Center Extreme Precipitation Tables as required by the Town of Newbury. Comparison of pre- and post-development stormwater runoff calculation results are summarized below in Table 1.

Subcatchment	Storm Frequency				
	2-Year	10-Year	100-Year		
Pre-Development	4.18	10.85	30.63		
Post-Development	3.55	10.71	29.38		

# Table 1: Comparison of Pre-Development and<br/>Post-Development Peak Runoff Rates (1)

1. Flow rates measured in cubic feet per second (cfs).

#### 2.3 Standard 3: Recharge

Site soils are mapped by the United States Department of Agriculture – Soil Conservation Service (SCS) (Essex Co. Massachusetts Southern Part Soil Survey, 1984) as being primarily Belgrade very fine sandy loam. Soil testing performed at the site generally indicated a fine loamy sand over coarse sand. Results were generally consistent with the SCS soil profiles. A 'C' Hydrologic Soil Group (HSG) was assigned to the soils for this analysis.

For C-type soils, the Stormwater Management Guidelines require that a recharge device be provided with a capacity equal to 0.25-inches times the impervious area. The minimum design groundwater recharge volume is 874 cf. This project utilizes Low Impact Development (LID) techniques which involve directing stormwater runoff from the proposed building roofs and portions of the driveways to "qualifying pervious areas". These areas are shown on the attached sketch (Attachment F). The LID credits claimed for this project (Credit 2 & 3) reduce the minimum required recharge volume by 162%, meaning the recharge requirement has been met (and exceeded). Calculations are enclosed (Attachment B).

#### 2.4 Standard 4: Water Quality

The minimum required water quality treatment volume (WQV) for the proposed residential development is one-inch times the area of the impervious surfaces due to the rapid infiltration rate of the underlying sandy soils. Runoff from most of the proposed roadway will be directed into the proposed constructed stormwater wetland. The constructed stormwater wetland is equipped with a sediment forebay to achieve 80% annual TSS removal and was sized to accommodate the WQV. The LID credits described in Section 2.3 were similarly used to reduce the required WQV by 40%. The reader is referred to Water Quality Volume Calculations provided in Attachment B.

As required by the Stormwater Management Standards, a Long-Term Pollution Prevention Plan has been prepared and can be found in Attachment C. In short, the plan identifies suitable practices for source control and pollution prevention measures.

#### 2.5 Standard 5: Land Uses with Higher Potential Pollutant Loads

In accordance with the Stormwater Management Standards, the proposed residential use is not considered a Land Use with Higher Potential Pollutant Loads. Therefore, this standard does not apply to this project.

#### 2.6 Standard 6: Critical Areas

The site does not discharge to any critical areas. Therefore, this standard does not apply to this project.

#### 2.7 Standard 7: Redevelopment and Other Projects Subject to the Standards only to the Maximum Extent Practicable

This project is entirely new development so this standard does not apply.

#### 2.8 Standard 8: Construction Period Pollution Prevention and Erosion and Sediment Control

The NPDES Construction General Permit requires that a Stormwater Pollution Prevention Plan (SWPPP) be prepared for any project disturbing over 1-acre of land. The proposed project will disturb approximately 5.6-acres of land. In accordance with the Massachusetts Stormwater Management Standards and the General Permit, a SWPPP will be prepared prior to land disturbance commencing.

Construction shall proceed in the following sequence:

#### **Roadway Construction**

- 1. Install Erosion Controls downhill of work areas. Inspection and maintenance of these Erosion Controls is required throughout the project as detailed below.
- 2. Clear & Grub roadway area.
- 3. Install construction entrance (rip rap) at Orchard Street for construction vehicles entering and exiting.
- 4. Bring roadway to rough grade.
- 5. Install water line and electric, cable and phone utilities.
- 6. Construct stormwater management features.
- 7. Fine grade roadway and pave.
- 8. Perform final landscaping.

#### Lot Development (Typical of 4 Lots)

- 1. Install Erosion Controls downhill of work areas. Inspection and maintenance of Erosion Controls is required throughout the project as detailed below.
- 2. Clear & Grub lot. Stockpile topsoil.
- 3. Install construction entrance (rip rap) along street line for construction vehicles entering and exiting.
- 4. Excavate foundation hole. Install foundation and first floor deck.
- 5. Backfill around the foundation.
- 6. Install building utilities, and rough grade site. Construct residence.

- 7. Construct septic system.
- 8. Install driveway and landscaping.

The proposed project includes a comprehensive set of mitigation measures to protect the surrounding sites from impacts due to construction. Prior to work commencing onsite, there will be a preconstruction conference with the contractor. The purpose of this meeting will be to coordinate the best methods for erosion and sedimentation control and other construction-related issues. The implementation of a comprehensive soil and erosion control plan will occur prior to any construction activities within the project area. In general, the following sequence of events will occur:

- Erosion and sedimentation control devices will be installed along the edge of the down-gradient side of the project area prior to construction as depicted on the site plan. In addition to providing for sedimentation deposition and reducing runoff during storm events, this barrier will limit the work area for the equipment operators.
- Erosion and sedimentation control devices will be inspected daily during periods of active construction and bi-weekly during the remainder of the construction period. Sediments will be removed from the barriers as soon as they reach a depth of 6-inches.
- Runoff from the site will be directed through sedimentation control barriers.
- During construction, disturbed areas will be kept to a minimum and vegetative stabilization of these areas will occur as soon as practicable.
- Temporary seeding, mulching, or other suitable stabilization measures will be used to protect exposed critical areas should unprotected soils remain exposed for prolonged periods.

Construction activities shall be monitored on-site by the construction supervisor to ensure that the soil erosion and sediment control features are installed properly, maintained, and to evaluate the need for additional erosion control and/or stabilization measures. The inspector will perform the following tasks:

- Supervise the installation and maintenance of the soil erosion and sediment control features.
- Evaluate the need for additional soil erosion and sediment control features.
- Scheduled inspections of erosion control features, including construction entrance, haybales, and dust control.
- Supervise and monitor temporary and permanent stabilization activities.

#### 2.9 Standard 9: Operation and Maintenance Plan

An Operations & Maintenance plan has been provided (Attachment D). The owner(s) of the new residences on Lots 1 through 4, acting through a homeowner's association, will be the parties responsible for operation and maintenance of the proposed stormwater management devices.

#### 2.10 Standard 10: Illicit Discharges

The submitted Long-Term Pollution Prevention Plan (Attachment C) specifies measures to prevent illicit discharges from entering the stormwater management system. Source control and response plans are also specified to prevent illicit discharges from being conveyed through the stormwater management system.

Consistent with the Massachusetts Stormwater Handbook, a signed Illicit Discharge Compliance Statement will be finalized prior to discharging stormwater to the post-construction stormwater BMP's. A draft copy of the Illicit Discharge Statement is provided (Attachment E).

## 3.0 SUMMARY

The proposed drainage system and site development plans for the four-lot residential development conforms to the MassDEP Stormwater Management Regulations. The proposed drainage system will treat and remove TSS and other pollutants throughout the project area and minimize erosion. Proper construction and operation and maintenance of the proposed drainage system are critical to its long-term performance. To that end, an Operations and Maintenance Plan and Long-Term Pollution Prevention Plan have been prepared and will be instituted.

## ATTACHMENT B STORMWATER COMPUTATIONS

- Low Impact Development Calculations
- Water Quality Volume Calculations
- TSS Removal Calculations



Phone: 978-927-5111; Fax: 978-927-5103

### LOW IMPACT DEVELOPMENT (LID) CREDIT CALCULATION

Job Name: 170 Orchard Street Job No: 2043 Date 1/4/2023 Designer SSM Checked By: RHG

SITE INF	ORMA	ΓΙΟΝ				
896,228	sf	(20.6 AC)				
41,950	sf	(4.7%)				
С	HSG					
0.25	in					
1	in	(rapid infiltration rate)				
874	cf	(41,950 sf * 0.25 in) / (12 in / ft)				
10,488	sf	(0.25) * (41,950 sf)				
3,496	cf	(41,950 sf * 1 in) / (12 in / ft)				
	REDIT	(LID 2):				
4		(house roofs directed to qualifying areas)				
2,092	sf					
8,368	sf	(4 * 2,092 sf)				
ROADWAY & DRIVEWAY (LID 3):						
8,603	sf	(paved areas directed to qualifying areas)				
RESULTS						
16,971	sf	(8,368 sf + 8,603 sf)				
24,979	sf	(41,950 sf - 16,971 sf)				
(540)	cf	(((10,488 sf - 16,971 sf) / 10,488 sf ) * 874 sf) (< 0, recharge requirement is met)				
2,082	sf	(24,979 sf * 1 in) / (12 in / ft)				
ent Reduct	ion Usii	ng Credits:				
162%	Reduc	ction				
40%	Reduc	ction				
	896,228 41,950 C 0.25 1 <b>874</b> 10,488 <b>3,496</b> <b>DOFTOP C</b> 4 2,092 8,368 <b>DWAY &amp; D</b> 8,603 <b>RES</b> 16,971 24,979 <b>(540)</b> <b>2,082</b> <b>ent Reduct</b> 162%	2,092 sf 8,368 sf				

Note: Ref. Masssachusetts Stormwater Handbook Volume 3, Chapter 1 - Documenting Compliance



Phone: 978-927-5111; Fax: 978-927-5103

### **BMP SIZING**

Job Name: 170 Orchard Street Job No: 2043 Date 1/4/2023 Designer SSM Checked By: RHG

#### **Constructed Stormwater Wetland:**

Tributary Impervious Area:	26,001 sf	(ref HydroCAD calculations)
BMP Required WQV:	2,167 cf	(26,001 sf * 1 in) / (12 in / ft)
Total Site Required WQV:	2,082 cf	(see LID Credit calculation)
BMP Design WQV:	2,167 cf	(greater of the two WQVs above)
Provided Storage Volume:	3,827 cf	(below lowest outlet, ref HydroCAD calculations)

#### INSTRUCTIONS:

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

3. After BMP is selected, TSS Removal and other Columns are automatically completed.

	Location:	P1a; P1b; P1c P1d; P1e; P1	f		
	В	С	D	Е	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
heet	Constructed Stormwater Wetland	0.80	1.00	0.80	0.20
moval Worksheet		0.00	0.20	0.00	0.20
		0.00	0.20	0.00	0.20
TSS Re Calculation		0.00	0.20	0.00	0.20
Cal		0.00	0.20	0.00	0.20
		Total T		Separate Form Needs to be Completed for Each Outlet or BMP Train	
	Project:	170 Orchard Street		-	
	Prepared By:			*Equals remaining load from	n previous BMP (E)
	· · · · ·	1/4/2023		which enters the BMP	
Non-automate	ed TSS Calculation Sheet				

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1

# ATTACHMENT C

LONG-TERM POLLUTION PREVENTION PLAN

### Long-Term Pollution Prevention Plan

Standard #4 of the MA DEP Stormwater Management Handbook requires that a Long-Term Pollution Prevention Plan (LTPPP) be prepared and incorporated into the longterm operation and maintenance plan of the projects stormwater management system. The purpose of the LTPPP is to identify potential sources of pollution that may affect the quality of stormwater discharges and to describe suggested practices to reduce pollutants in stormwater discharges.

<u>Good housekeeping practices</u> - The subject property owners are to keep the site in a neat and orderly condition so that pollutants are not conveyed to the stormwater drainage system. Materials swept, blown or washed into the system can decrease the system's effectiveness and could eventually be conveyed into the nearby wetland resource area. Some examples of good housekeeping practices are pavement sweeping, litter control, contained outdoor waste and proper cigarette disposal, and protected material storage areas. The property owners should assign responsibilities to personnel to keep the property in a neat and orderly condition.

<u>Provisions for storing materials and waste products inside or under cover</u> – There are no exterior (un-covered) storage areas associated with the project site.

<u>Requirements for routine inspections and maintenance of stormwater BMP's</u> -Consistent with Standard 9 of the Massachusetts Stormwater Management Regulations, an Operation and Maintenance Plan has been provided in the Stormwater Management Report. The plan details routine inspection and maintenance of the stormwater BMP's along with associated record keeping forms.

<u>Spill prevention and response plans</u> – Sources of potential spill hazards include vehicle fluids and fuels, pesticides, paints, solvents, and liquid cleaning products. The majority of the spill hazards would likely occur within the building and would not enter the stormwater drainage system. However, there are spill hazards from vehicle fluids and fuels located outside of the buildings. These exterior spill hazards have the potential to enter the stormwater drainage system and are to be addressed as follows:

- 1) Spill hazards of pesticides, paints, and solvents shall be remediated using the Manufacturers' recommended spill cleanup protocol.
- 2) Vehicle fluid and fuel spills shall be remediated according to local and state regulations governing fuel spills.
- 3) The property owners shall have the following equipment and materials on hand to address a spill clean-up: brooms, dust-pans, mops, rags, gloves, trash bags, and trash containers.
- 4) Spills of toxic or hazardous materials shall be reported to the Massachusetts Department of Environmental Protection at 1-888-304-1133.

<u>Provisions for maintenance of lawns, garden, and other landscaped areas</u> - It should be a general goal of the subject property owners to achieve a high quality of well-groomed and stable landscape that evolves throughout the changing seasons and overall condition of the property. All landscaped areas are to be maintained with dense vegetative growth or a layer of mulch so as to minimize sediment transport. Litter and waste is to be removed weekly from these areas and disposed of properly.

<u>Requirements for storage and use of fertilizer, herbicides, and pesticides</u> - Fertilizers, herbicides, and pesticides are not to be stored on site or within the buildings. Should use of same become necessary, application should be performed by a state licensed contractor in accordance with the manufacturer's label instruction and when environmental conditions are conducive to product application. Chemical controls should be used as a last resort to organic and biological control methods.

<u>Pet waste management provisions</u> - All pet waste is to be scooped up, sealed in a plastic bag, and disposed of properly in the garbage. Never deposit pet waste in the stormwater management system for it contains high levels of bacteria.

<u>Provisions for operation and management of septic systems</u> – The on-site septic system should be inspected and maintained on a regular basis. Discharge or ponding of effluent at the ground surface may indicate system failure and should be resolved immediately.

<u>Snow disposal and deicing chemicals</u> – The individual property owners will be responsible for the clearing of their individual driveways and building entrances. The owners may be required to use a de-icing agent such as salt or calcium chloride to maintain a safe walking surface. The de-icing agent for the walkways and building entrances should be kept on site within a building (i.e. garage).

# ATTACHMENT D

OPERATION & MAINTENANCE PLAN

## **OPERATION & MAINTENANCE PLAN**

### 170 Orchard Street Residential Development

#### System Owner:

Estate of Lewis Bulgaris (or Successor)

#### Party Responsible for O&M:

The individual homeowners for each lot will be responsible for the operation and maintenance of their respective on-site stormwater management features as outlined in this Operation and Maintenance (O&M) Plan. Should ownership of the property change, the succeeding owners shall have those responsibilities. A homeowners association (HOA) will contract-out maintenance of common utilities and stormwater BMPs.

Note: The system inspectors should note that drainage pipes, manholes, and treatment devices are considered "confined spaces" subject to strict OSHA standards regarding safe entry. Confined spaces present inherent hazards to workers. Only appropriately trained staff with appropriate safety equipment and monitors may enter confined spaces, and then only with a specific entry permit. Also, this work may pose hazards to workers, such as soft ground, flowing or standing water, snakes and rodents. Again, only appropriately trained staff with the necessary safety equipment should undertake such work.

#### Post-Development Operation and Maintenance

The stormwater management system consists of a series of catchbasins, drain manholes, pipes, a constructed stormwater wetland, and several "qualifying pervious areas" (QPAs). Roof runoff is conveyed to the pervious areas via gutters, downspouts, and PVC roof leaders. Stormwater from the proposed roadway is directed into the constructed stormwater wetland via catchbasins and / or culvert pipes.

Inspection of the drainage system components are to be performed by the System Owner or their designee during the first year of operation on a quarterly basis. The inspection frequency can be reduced after the first year to annual inspections provided that the quarterly inspections do not indicate the need for more frequent inspections. If more frequent inspections become appropriate at any time, they should be implemented. Inspections should be documented by taking necessary notes, measurements, photographs, and retaining service receipts. The following inspections are required of the system owner:

<u>Roadway</u> - Remove debris from the roadway as it accumulates, as part of normal site clean-up. Weekly patrolling for litter is recommended. Sand from ice control should be removed monthly via a street sweeper during the winter season. Significant oil leaks should be swept up and disposed of using oil-absorbent material as they are

discovered. Any oil spills or leaks that reach the catchbasins must be reported to the Massachusetts DEP oil spill hotline.

<u>Catchbasins & Drain Manholes</u> - Remove the grate or cover and visually inspect for corrosion and structural damage. Inspect pipe inlets and bottoms for signs of infiltration or inflow. The grate or cover and hoods on the catchbasins should be inspected on a quarterly basis during the first and year and semi-annual thereafter. Cleaning of the catchbasins should be done on a yearly basis and by a vacuum truck or clamshell. While cleaning, if a layer of oil is observed floating on the water surface, place an oil-absorbent pillow on the surface, allow to soak and remove. Repeat this process until the oil layer is removed. Alternatively, have the oil layer pumped out by a licensed disposal contractor and appropriately disposed of. The oil absorbent pillows must be drummed for disposal by a licensed disposal contractor.

<u>Constructed Stormwater Wetland (CSW)</u> – The CSW should be inspected at least quarterly during the first two years, and once a year thereafter. The inspection should determine the amount of sediment accumulation in the forebay and micropool. Check to make sure the plants are healthy and in good condition. Access areas and embankments should be mowed twice a year. The CSW should be inspected after major storms to ensure proper function and stabilization. Water levels should be recorded over several days. Follow the schedule below for maintenance of the CSW.

Schedule	Activity
Annually (Quarterly During First Two Years)	<ul> <li>Inspect inflow area and overflow spillway for sediment accumulation. Remove any accumulated sediment or debris. Silt shall be removed as it accumulates.</li> <li>Inspect for erosion, subsidence, or cracking of embankments.</li> <li>Inspect for dead or dying vegetation. Replace vegetation as needed with plants from original plant list.</li> </ul>
Regularly (Monthly)	<ul> <li>Remove accumulated trash and debris.</li> <li>Weed and prune as necessary to prevent invasive species from taking over and to allow the desired vegetation to thrive.</li> </ul>
As Needed (Following Construction)	<ul> <li>Water to promote plant growth and survival, especially during the first two years and during dry spells.</li> <li>Inspect plants following major storm events to ensure proper function and stabilization. Water levels should subside within a day or two after large storms.</li> </ul>

Record date, description, and contractor (if applicable) for all structural repairs and plant

replacement.

<u>Qualifying Pervious Areas</u> – During the first year, QPAs should be inspected after major storms to ensure proper function and stabilization. After the first year QPAs should be inspected annually for erosion, sediment accumulation, or subsidence. All trash and debris should be removed from the surrounding area. Silt should be removed as it accumulates.

#### Snow Storage

The new roadway is designed with 22 feet pavement width and two-foot shoulders throughout. This should provide ample room to maintain travel lanes with snow cast along the edge of the roadway. In the event of significant snow, clearing of snow banks at intersections to provide increased visibility may be necessary. In these instances, snow should be moved less than 100 feet to a more convenient location.

## **POST-CONSTRUCTION MAINTENANCE INSPECTION FORM**

170 Orchard Street Residential Development

Inspections/reports must be completed quarterly for the first year of operation. Inspection frequency can be reduced after the first year to annual inspections provided that the quarterly inspections do not indicate the need for more frequent inspections.

#### Inspection

Type:	
-------	--

Quarterly Inspection
 Annual Inspection
 Emergency Inspection

 (i.e. Ponding, Flooding, and/or Severe Erosion)

Date: \_\_\_\_\_

Weather Conditions:

BMP Inspection Areas	Satisfactory	Unsatisfactory	Comments/Corrective Action Required
Catchbasins, Manholes & Pining			
Constructed Stormwater Wetland			
- Inflow area and Overflow Spillway			
- Erosion, Subsidence, or Cracking of Embankments			
- Dead or Dying Vegetation			
- Prune and Weed Stone Berm			
- Housekeeping / Trash			
Downspouts & Roof Leaders			
Qualifying Pervious Areas			
Other Necessary Controls			

Site Notes:

# ATTACHMENT E

ILLICIT DISCHARGE STATEMENT

## ILLICIT DISCHARGE COMPLIANCE STATEMENT

I verify that no illicit discharges exist from the 170 Orchard Street residential development. Through the implementation of Long-Term Pollution Prevention Plan and Operation and Maintenance Plan, measures are set forth to prevent illicit discharges from entering the stormwater management drainage system.

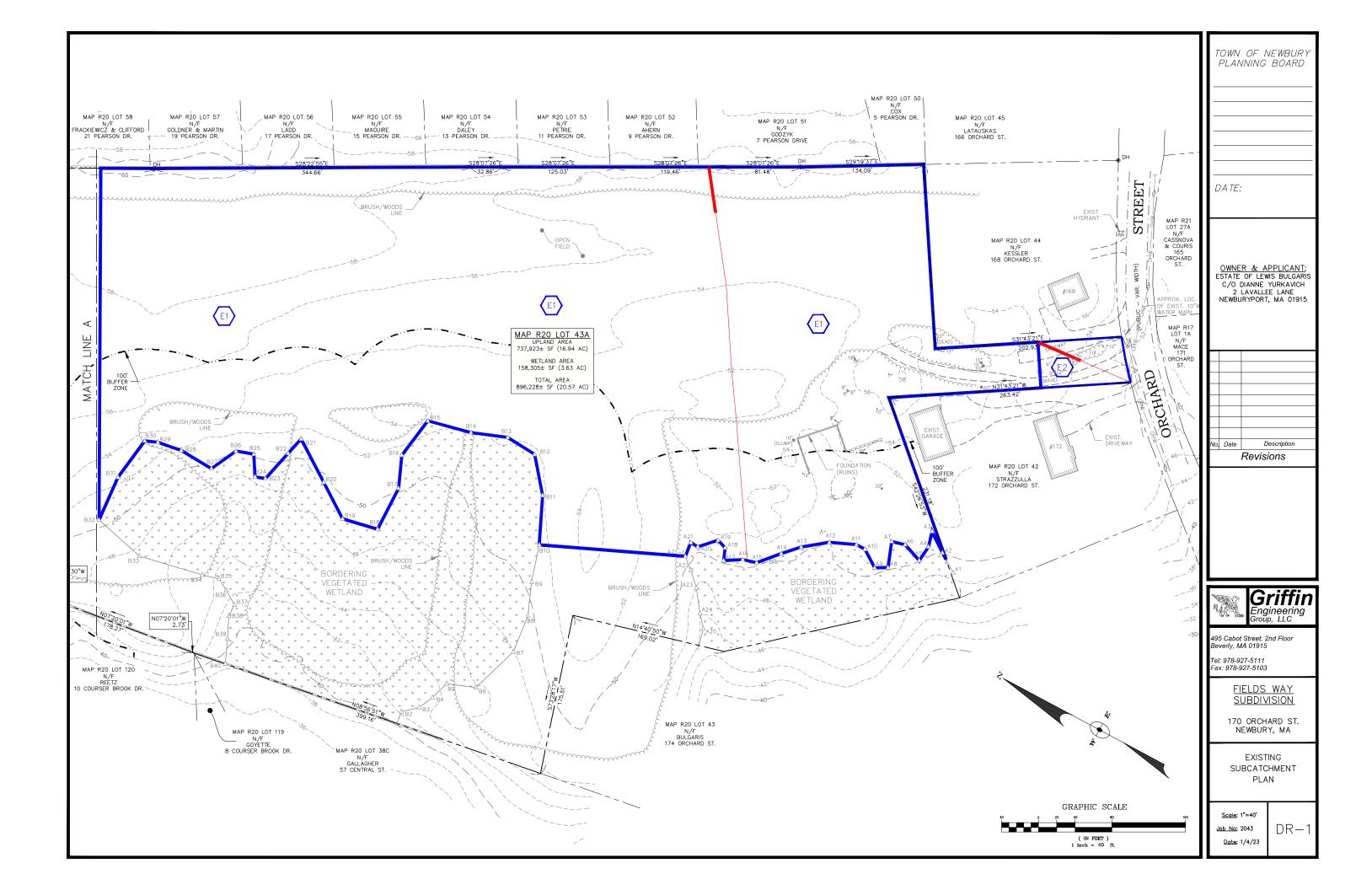
Signature	Print Name	Date
Title	Company	
Signature	Print Name	Date
Title	Company	

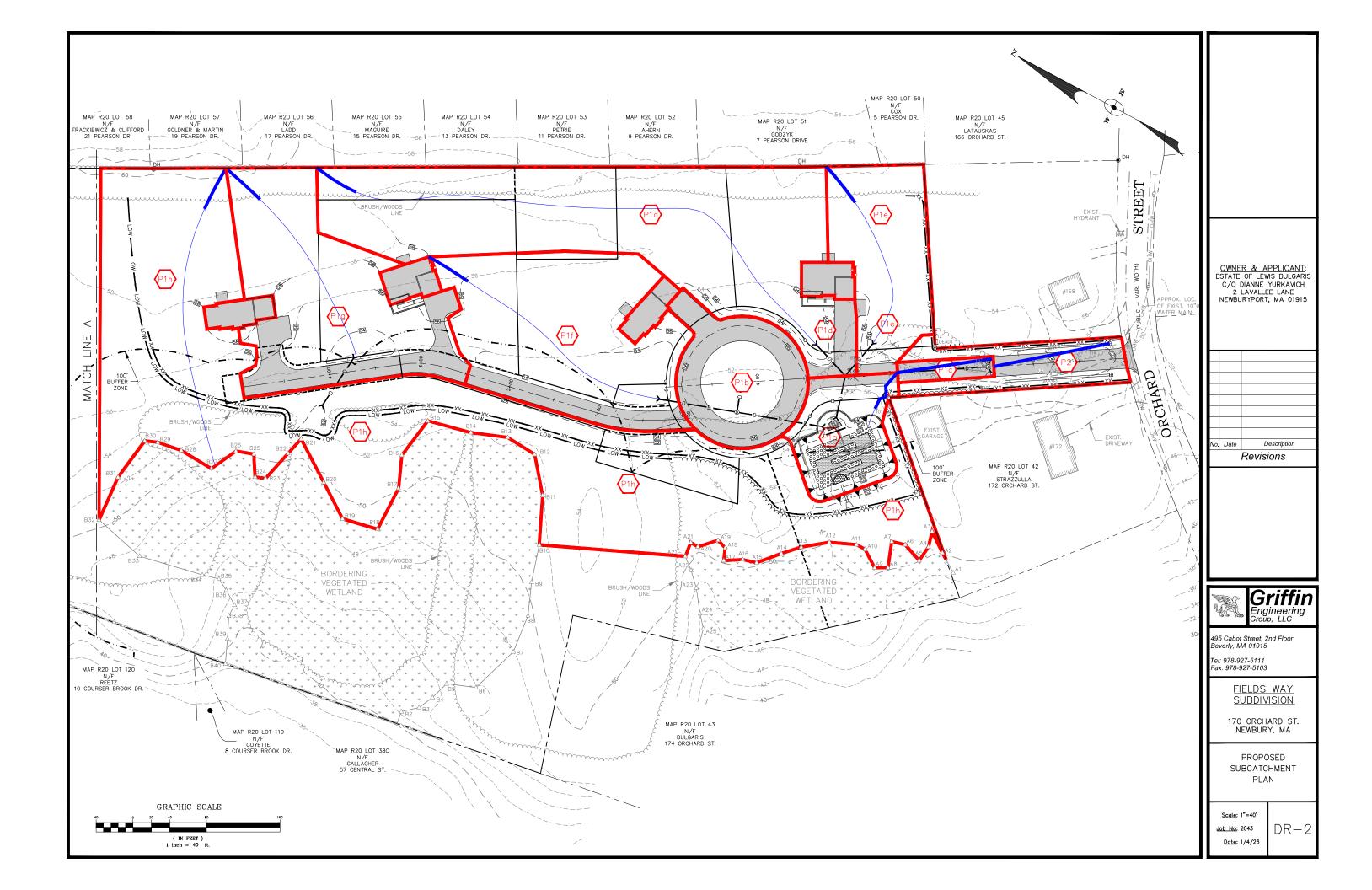
Note: This certification must be signed before stormwater is conveyed to the proposed stormwater drainage system in accordance with Standard 10 of the Massachusetts Stormwater Management Standards.

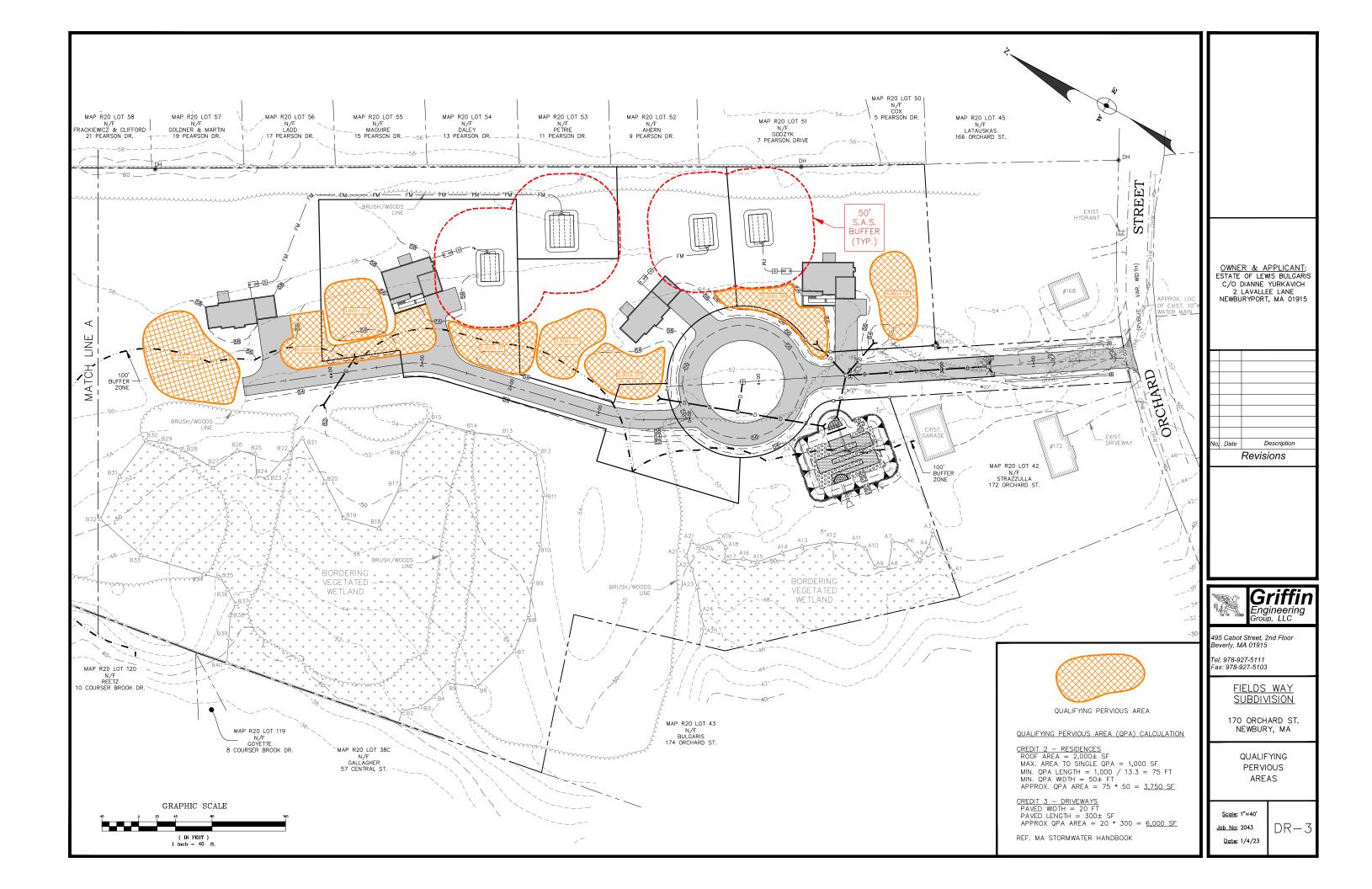
# ATTACHMENT F

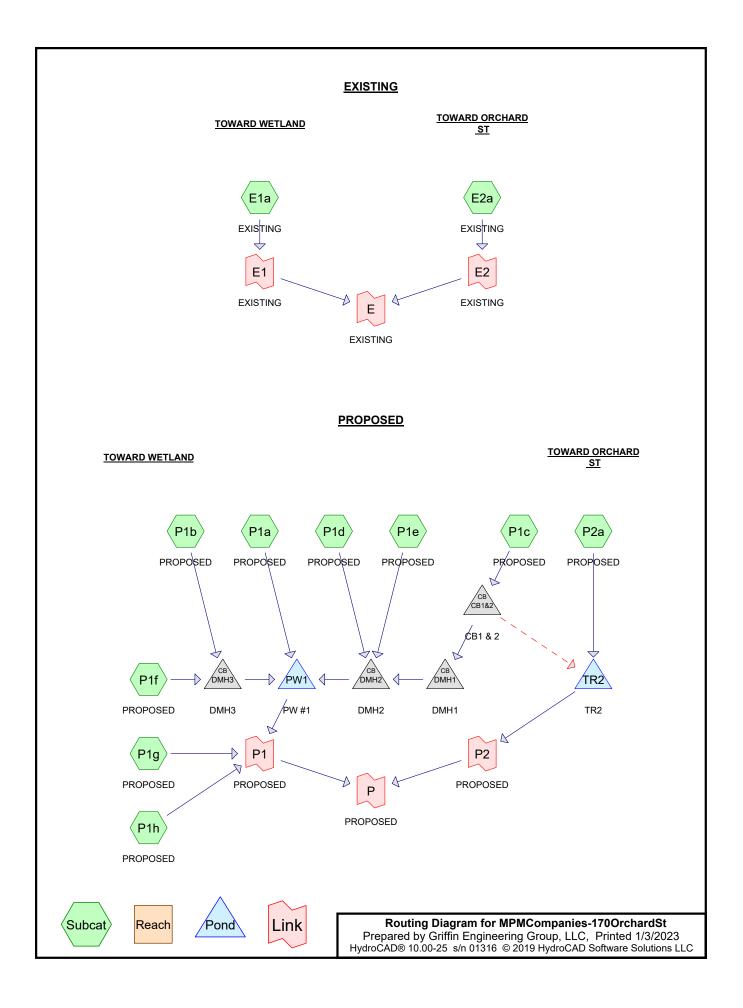
STORMWATER ANALYSIS

- Subcatchment Plans, DR-1 & DR-2 (Reduced Size, 11x17)
- HydroCAD Calculations
  - (2-, 10-, & 100-Year Storm Events)
- Qualifying Pervious Area Sketch (Reduced Size, 11x17)









## Summary for Subcatchment E1a: EXISTING

Runoff = 4.12 cfs @ 12.38 hrs, Volume= 23,184 cf, Depth= 0.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

A	rea (sf)	CN D	escription		
3	33,614	70 V	Voods, Go	od, HSG C	
3	333,614		00.00% Pe	ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.2	50	0.0140	0.06		Sheet Flow,
10.5	374	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
24.7	424	Total			

### Summary for Subcatchment E2a: EXISTING

Runoff = 0.07 cfs @ 12.20 hrs, Volume= 326 cf, Depth= 0.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

_	A	rea (sf)	CN E	escription				
	4,694 70 Woods, Good, HSG C							
		4,694	1	00.00% Pe	ervious Are	a		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
-	12.3	50	0.0200	0.07		Sheet Flow,		
	0.9	40	0.0200	0.71		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps		
	13.2	90	Total					

## Summary for Subcatchment P1a: PROPOSED

Runoff = 0.38 cfs @ 12.09 hrs, Volume= 1,212 cf, Depth= 1.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

 Type III 24-hr
 2-yr Rainfall=3.21"

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 1/3/2023

 C
 Page 3

Prepared by Griffin Engine	
HydroCAD® 10.00-25 s/n 0131	6 © 2019 HydroCAD Software Solutions LLC

rea (sf)	CN E	Description							
11,421	74 >	74 >75% Grass cover, Good, HSG C							
1,131	98 F	Paved park	ing, HSG C						
12,552	76 V	Veighted A	verage						
11,421	-								
1,131	g	0.01% Impe	ervious Area	а					
			<b>.</b>						
•				Description					
(teet)			(cts)						
16	0.0300	1.12		Sheet Flow,					
				Smooth surfaces n= 0.011 P2= 3.21"					
34	0.0600	0.21		Sheet Flow,					
				Grass: Short n= 0.150 P2= 3.21"					
21	0.1200	2.42		Shallow Concentrated Flow,					
				Short Grass Pasture Kv= 7.0 fps					
				Direct Entry, 6' (MIN.)					
71	Total								
	11,421 1,131 12,552 11,421 1,131 Length (feet) 16 34 21	11,421       74       >         1,131       98       F         12,552       76       V         11,421       9         1,131       9         1,131       9         1,131       9         Length       Slope         (feet)       (ft/ft)         16       0.0300         34       0.0600         21       0.1200	11,421         74         >75% Grass           1,131         98         Paved park           12,552         76         Weighted A           11,421         90.99% Per           1,131         9.01% Impe           Length         Slope         Velocity           (feet)         (ft/ft)         (ft/sec)           16         0.0300         1.12           34         0.0600         0.21           21         0.1200         2.42	11,421       74       >75% Grass cover, Go         1,131       98       Paved parking, HSG C         12,552       76       Weighted Average         11,421       90.99% Pervious Area         1,131       9.01% Impervious Area         1,6       0.0300       1.12         34       0.0600       0.21         21       0.1200       2.42					

## Summary for Subcatchment P1b: PROPOSED

2,945 cf, Depth= 2.01"

Runoff = 0.95 cfs @ 12.09 hrs, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

A	rea (sf)	CN	Description					
	7,216	74	>75% Gras	s cover, Go	bod, HSG C			
	10,401	98	Paved parking, HSG C					
	17,617	88	88 Weighted Average					
	7,216		40.96% Pei	vious Area	l			
	10,401	:	59.04% Imp	pervious Are	ea			
Tc	Length	Slope	,	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
6.0					Direct Entry, 6' (MIN.)			

## Summary for Subcatchment P1c: PROPOSED

Runoff = 0.17 cfs @ 12.08 hrs, Volume= 572 cf, Depth= 2.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

 Area (sf)	CN	Description
2,307	98	Paved parking, HSG C
 2,307		100.00% Impervious Area

				roup, LLC		Type	Drinted	1/3/2023		
					) Software Solu	itions LLC	Finited	Page 4		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)							
6.0					Direct Entry	/, 6' (MIN.)				
	Summary for Subcatchment P1d: PROPOSED									
Runoff	=	1.08 cfs	s@ 12.3	9 hrs, Volu	ime=	5,938 cf, De	epth= 1.04"			
Type III 2	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"									
A	rea (sf)		escription							
	49,295 2,363 15,500 1,088	98 U 70 V	Inconnecte Voods, Go	s cover, Go ed pavemer od, HSG C ed roofs, HS						
68,246         74         Weighted Average           64,795         94.94% Pervious Area           3,451         5.06% Impervious Area           3,451         100.00% Unconnected										
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
12.3	50	0.0200	0.07	· /	Sheet Flow					
14.3	570	0.0090	0.66		Shallow Co	it underbrush <b>ncentrated F</b> Pasture Kv=		"		
26.6	620	Total					•			

Type III 24-hr 2-yr Rainfall=3.21"

26.6 620 Total

**MPMCompanies-170OrchardSt** 

# Summary for Subcatchment P1e: PROPOSED

Runoff =

0.40 cfs @ 12.26 hrs, Volume= 1,861 cf, Depth= 1.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

Area (sf)	CN	Adj	Description
16,470	74		>75% Grass cover, Good, HSG C
700	98		Unconnected pavement, HSG C
3,133	70		Woods, Good, HSG C
1,088	98		Unconnected roofs, HSG C
21,391	75	74	Weighted Average, UI Adjusted
19,603			91.64% Pervious Area
1,788			8.36% Impervious Area
1,788			100.00% Unconnected

Prepare	d by Grit	ffin Engir		roup, LLC	Type III 24-hr 2-yr Rainfall=3.21"Printed 1/3/2023O Software Solutions LLCPage 5			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
14.2	50	0.0140	0.06		Sheet Flow,			
3.3	170	0.0150	0.86		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps			
17.5	220	Total						
	Summary for Subcatchment P1f: PROPOSED							
Runoff	=	1.12 cf	s @ 12.1	5 hrs, Volu	ime= 4,169 cf, Depth= 1.16"			
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"							
A	rea (sf)			ription				
	35,159 4,913	74 98			ver, Good, HSG C avement, HSG C			
	2,008	98 98			bofs, HSG C			
	1,088	98			bofs, HSG C			
	43,168				age, UI Adjusted			
	35,159		-	5% Perviou				
	8,009			5% Impervi				
	8,009		100.	00% Uncor	inected			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	1			
4.3	50	0.0400	0.20		Sheet Flow,			
	0.50		a <b>-</b> a		Grass: Short n= 0.150 P2= 3.21"			
6.0	250	0.0100	0.70		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps			
10.3	300	Total						
		S	ummary	for Subo	catchment P1g: PROPOSED			

Runoff = 0.88 cfs @ 12.28 hrs, Volume= 4,081 cf, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

Area (sf)	CN	Adj	Description
26,694	74		>75% Grass cover, Good, HSG C
8,603	98		Unconnected pavement, HSG C
2,788	70		Woods, Good, HSG C
1,088	98		Unconnected roofs, HSG C
1,004	98		Unconnected roofs, HSG C
40,177	80	77	Weighted Average, UI Adjusted
29,482			73.38% Pervious Area
10,695			26.62% Impervious Area
10,695			100.00% Unconnected

				roup, LLC 9 HydroCAE	Printed 1/3/2023     O Software Solutions LLC				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
16.2	50	0.0100	0.05	\$ <b>1</b>	Sheet Flow,				
2.5	200	0.0350	1.31		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps				
18.7	250	Total							
	Summary for Subcatchment P1h: PROPOSED								
Runoff	=	1.89 cf	s@ 12.3	1 hrs, Volu	ıme= 9,553 cf, Depth= 0.94"				
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr  2-yr Rainfall=3.21"								
	rea (sf)		escription						
	47,534 73,953			s cover, Go od, HSG C	ood, HSG C				
	1,004				SG C				
	1,004         98         Unconnected roofs, HS           122,491         72         Weighted Average           121,487         99.18% Pervious Area           1,004         0.82% Impervious Area           1,004         100.00% Unconnected			verage vious Area ervious Area	a				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
16.2	50	0.0100	0.05		Sheet Flow,				
3.7 0.7	220 66	0.0200 0.1000	0.99 1.58		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps <b>Shallow Concentrated Flow,</b>				
20.6	336	Total			Woodland Kv= 5.0 fps				
20.0	000								

Type III 24-hr 2-yr Rainfall=3.21"

## Summary for Subcatchment P2a: PROPOSED

Runoff = 0.41 cfs @ 12.09 hrs, Volume= 1,275 cf, Depth= 1.48"

MPMCompanies-170OrchardSt

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.21"

Area (sf)	CN	Description
7,205	74	>75% Grass cover, Good, HSG C
3,154	98	Unconnected pavement, HSG C
10,359	81	Weighted Average
7,205		69.55% Pervious Area
3,154		30.45% Impervious Area
3,154		100.00% Unconnected

MPMCompanies-170OrchardSt Prepared by Griffin Engineering Group, LLC HydroCAD® 10.00-25 s/n 01316 © 2019 HydroCAD Softwar				Group, LLC		Type III 24-hr 2-yr Rainfall=3.2 Printed 1/3/20 ons LLC Page	23
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0	6.0 Direct Entry, 6' (MIN.)						
	Summary for Pond CB1&2: CB1 & 2						
Inflow Outflow Primary Seconda	Inflow Area = $2,307 \text{ sf},100.00\%$ Impervious, Inflow Depth = $2.98"$ for 2-yr eventInflow = $0.17 \text{ cfs}$ @ $12.08 \text{ hrs}$ , Volume= $572 \text{ cf}$ Outflow = $0.17 \text{ cfs}$ @ $12.08 \text{ hrs}$ , Volume= $572 \text{ cf}$ Primary = $0.17 \text{ cfs}$ @ $12.08 \text{ hrs}$ , Volume= $572 \text{ cf}$ Secondary = $0.00 \text{ cfs}$ @ $0.00 \text{ hrs}$ , Volume= $0 \text{ cf}$ Routing by Dyn-Stor-Ind method, Time Span= $0.00 \text{ hrs}, \text{ dt} = 0.01 \text{ hrs} / 2$						
Peak Ĕle Flood El	ev= 53.55' lev= 55.90'	@ 12.09	) hrs				
<u>Device</u> #1	Routing Primary		53.40' ' I	L= 5.0' RC	<b>d Culvert X 2.0</b> P, sq.cut end pr Invert= 53.40' /	00 rojecting, Ke= 0.500 / 53.20' S= 0.0400 '/' Cc= 0.900 raight & clean, Flow Area= 0.55 sf	
#2	Seconda	ry	55.90' 2   	<b>2.0' long x</b> Head (feet) 2.50 3.00 3	<b>2.0' breadth Br</b> 0.20 0.40 0.60 3.50 sh) 2.54 2.61 2	Foad-Crested Rectangular Weir X 2.00           0         0.80         1.00         1.20         1.40         1.60         1.80         2.00           2.61         2.60         2.66         2.70         2.77         2.89         2.88	
	Primary OutFlow Max=0.16 cfs @ 12.08 hrs HW=53.55' TW=53.43' (Dynamic Tailwater)						
					HW=53.40' TV ols 0.00 cfs)	W=49.00' (Dynamic Tailwater)	
Summary for Pond DMH1: DMH1							

Inflow Area :	=	2,307 sf,100.00% Impervious,	Inflow Depth = 2.98" for 2-yr event
Inflow =	=	0.17 cfs @ 12.08 hrs, Volume=	572 cf
Outflow =	=	0.17 cfs @ 12.08 hrs, Volume=	572 cf, Atten= 0%, Lag= 0.0 min
Primary =	=	0.17 cfs @ 12.08 hrs, Volume=	572 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 53.43' @ 12.09 hrs Flood Elev= 56.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	53.20'	12.0" Round Culvert
			L= 150.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 53.20' / 52.30' S= 0.0060 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

Primary OutFlow Max=0.16 cfs @ 12.08 hrs HW=53.43' TW=52.76' (Dynamic Tailwater) ☐ 1=Culvert (Outlet Controls 0.16 cfs @ 1.86 fps)

## Summary for Pond DMH2: DMH2

Inflow Area	=	91,944 sf,	8.21% Impervious,	Inflow Depth = 1.09"	for 2-yr event
Inflow =	=	1.48 cfs @	12.36 hrs, Volume=	8,372 cf	
Outflow =	=	1.48 cfs @	12.36 hrs, Volume=	8,372 cf, Atte	en= 0%, Lag= 0.0 min
Primary =	=	1.48 cfs @	12.36 hrs, Volume=	8,372 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 53.00' @ 12.36 hrs Flood Elev= 56.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	52.30'	12.0" Round Culvert
			L= 44.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 52.30' / 52.00' S= 0.0068 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

Primary OutFlow Max=1.48 cfs @ 12.36 hrs HW=53.00' TW=51.31' (Dynamic Tailwater) -1=Culvert (Barrel Controls 1.48 cfs @ 3.53 fps)

## Summary for Pond DMH3: DMH3

Inflow Area =	60,785 sf, 30.29% Impervious,	Inflow Depth = 1.40" for 2-yr event
Inflow =	1.95 cfs @ 12.12 hrs, Volume=	7,114 cf
Outflow =	1.95 cfs @ 12.12 hrs, Volume=	7,114 cf, Atten= 0%, Lag= 0.0 min
Primary =	1.95 cfs @ 12.12 hrs, Volume=	7,114 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 53.34' @ 12.12 hrs Flood Elev= 55.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	52.50'	12.0" Round Culvert
			L= 92.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 52.50' / 52.00' S= 0.0054 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

Primary OutFlow Max=1.95 cfs @ 12.12 hrs HW=53.34' TW=50.75' (Dynamic Tailwater) ☐ 1=Culvert (Barrel Controls 1.95 cfs @ 3.75 fps)

## Summary for Pond PW1: PW #1

Inflow Area =	165,281 sf, 16.39% Impervious,	Inflow Depth = 1.21" for 2-yr event
Inflow =	3.18 cfs @ 12.13 hrs, Volume=	16,698 cf
Outflow =	1.56 cfs @ 12.62 hrs, Volume=	12,848 cf, Atten= 51%, Lag= 29.1 min
Primary =	1.56 cfs @ 12.62 hrs, Volume=	12,848 cf

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 51.49' @ 12.62 hrs Surf.Area= 4,597 sf Storage= 5,962 cf Flood Elev= 54.00' Surf.Area= 7,326 sf Storage= 20,944 cf

Plug-Flow detention time= 181.1 min calculated for 12,848 cf (77% of inflow) Center-of-Mass det. time= 92.3 min ( 949.2 - 856.9 )

Volume	Inv	vert Avail.Sto	rage Storage	Description		
#1	50.	00' 20,9	44 cf Custom	4 cf Custom Stage Data (Prismatic)Listed below (Recalc)		
Elevatio (fee 50.0 51.0 52.0	et) 00 00	Surf.Area (sq-ft) 3,450 4,204 5,015	Inc.Store (cubic-feet) 0 3,827 4,610	Cum.Store (cubic-feet) 0 3,827 8,437		
53.0		6,337	5,676	14,113		
54.0	00	7,326	6,832	20,944		
Device	Routing	Invert	Outlet Device	S		
#1	Primary	53.25'	Head (feet) 0 2.50 3.00 3.5 Coef. (English	.20 0.40 0.60 50 4.00 4.50 5	70 2.69 2.68 2.68 2.66 2.64 2.64	
#2	Primary	51.00'	<b>10.0" Round</b> L= 20.0' RCF Inlet / Outlet In	Culvert X 2.00 P, sq.cut end pro nvert= 51.00' / 5		

Primary OutFlow Max=1.56 cfs @ 12.62 hrs HW=51.49' TW=0.00' (Dynamic Tailwater) -1=Broad-Crested Rectangular Weir (Controls 0.00 cfs) -2=Culvert (Inlet Controls 1.56 cfs @ 2.37 fps)

#### Summary for Pond TR2: TR2

Inflow Area =	10,359 sf, 30.45% Impervious,	Inflow Depth = 1.48" for 2-yr event
Inflow =	0.41 cfs @ 12.09 hrs, Volume=	1,275 cf
Outflow =	0.13 cfs @ 11.98 hrs, Volume=	1,275 cf, Atten= 68%, Lag= 0.0 min
Discarded =	0.13 cfs @ 11.98 hrs, Volume=	1,275 cf
Primary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 49.75' @ 12.44 hrs Surf.Area= 684 sf Storage= 205 cf Flood Elev= 52.00' Surf.Area= 2,844 sf Storage= 1,957 cf

Plug-Flow detention time= 7.6 min calculated for 1,275 cf (100% of inflow) Center-of-Mass det. time= 7.6 min (846.9 - 839.4)

Type III 24-hr 2-yr Rainfall=3.21" Printed 1/3/2023 Page 10

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Volume	Invert	Avail.Stora	ge Storage Description
#1	51.00'	705	5 cf 3.00'W x 114.00'L x 1.00'H Prismatoid Z=3.0
#2	49.00'	274	cf 3.00'W x 114.00'L x 2.00'H Prismatoid
			684 cf Overall x 40.0% Voids
		979	9 cf x 2.00 = 1,957 cf Total Available Storage
Device	Routing	Invert (	Outlet Devices
#1	Primary	51.90'	20.0' long x 6.0' breadth Broad-Crested Rectangular Weir
	-	I	Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
		(	Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65
			2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83
#2	Discarded	49.00'	8.270 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded 8.270 in/hr Extilitration over Surface area Phase-In= 0.01

Discarded OutFlow Max=0.13 cfs @ 11.98 hrs HW=49.03' (Free Discharge) -2=Exfiltration (Exfiltration Controls 0.13 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=49.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

#### Summary for Link E: EXISTING

Inflow Area :	=	338,308 sf,	0.00% Impervious,	Inflow Depth = 0.83"	for 2-yr event
Inflow =	=	4.18 cfs @ 1	12.38 hrs, Volume=	23,510 cf	
Primary =	=	4.18 cfs @ 1	12.38 hrs, Volume=	23,510 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link E1: EXISTING

Inflow Are	a =	333,614 sf,	0.00% Impervious,	Inflow Depth = 0.83"	for 2-yr event
Inflow	=	4.12 cfs @ 1	12.38 hrs, Volume=	23,184 cf	
Primary	=	4.12 cfs @ 1	12.38 hrs, Volume=	23,184 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link E2: EXISTING

Inflow Area	a =	4,694 sf,	0.00% Impervious,	Inflow Depth = 0.83"	for 2-yr event
Inflow	=	0.07 cfs @ 1	12.20 hrs, Volume=	326 cf	
Primary	=	0.07 cfs @ 1	12.20 hrs, Volume=	326 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link P: PROPOSED

338,308 sf, 12.40% Impervious, Inflow Depth = 0.94" for 2-yr event Inflow Area = Inflow 3.55 cfs @ 12.47 hrs, Volume= 26,482 cf = 3.55 cfs @ 12.47 hrs, Volume= 26,482 cf, Atten= 0%, Lag= 0.0 min Primary =

# Summary for Link P1: PROPOSED

Inflow Area	a =	327,949 sf, 11.83% Impervious, Inflow Depth = 0.97" for 2-yr event	
Inflow	=	3.55 cfs @ 12.47 hrs, Volume= 26,482 cf	
Primary	=	3.55 cfs @12.47 hrs, Volume=26,482 cf, Atten= 0%, Lag= 0.0 m	nin

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

## Summary for Link P2: PROPOSED

Inflow Area	a =	10,359 sf,	30.45% Impervious,	Inflow Depth = 0.00"	for 2-yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	-
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

## Summary for Subcatchment E1a: EXISTING

Runoff = 10.72 cfs @ 12.37 hrs, Volume= 55,173 cf, Depth= 1.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

A	rea (sf)	CN E	Description		
3	33,614	70 V	Voods, Go	od, HSG C	
3	33,614	100.00% Pervious Area			а
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.2	50	0.0140	0.06		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.21"
10.5	374	0.0140	0.59		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
24.7	424	Total			

### Summary for Subcatchment E2a: EXISTING

Runoff = 0.19 cfs @ 12.19 hrs, Volume= 776 cf, Depth= 1.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

	Area (sf)	CN E	Description		
	4,694	70 V	Voods, Go	od, HSG C	
	4,694	1	00.00% Pe	ervious Are	a
To (min		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.3	3 50	0.0200	0.07	· · · ·	Sheet Flow,
0.9	9 40	0.0200	0.71		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
13.2	2 90	Total			

## Summary for Subcatchment P1a: PROPOSED

Runoff = 0.84 cfs @ 12.09 hrs, Volume= 2,592 cf, Depth= 2.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

 Type III 24-hr
 10-yr Rainfall=4.93"

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A	rea (sf)	CN E	Description					
	11,421	74 >	>75% Grass cover, Good, HSG C					
	1,131	98 F	aved park	ing, HSG C	;			
	12,552	76 V	Veighted A	verage				
	11,421	9	0.99% Per	vious Area				
	1,131	9	.01% Impe	ervious Area	а			
_								
Тс	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
0.2	16	0.0300	1.12		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.21"			
2.7	34	0.0600	0.21		Sheet Flow,			
					Grass: Short			
0.1	21	0.1200	2.42		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
3.0					Direct Entry, 6' (MIN.)			
6.0	71	Total						

## Summary for Subcatchment P1b: PROPOSED

5,289 cf, Depth= 3.60"

Runoff = 1.67 cfs @ 12.09 hrs, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

A	rea (sf)	CN	Description			
	7,216	74	>75% Gras	s cover, Go	bod, HSG C	
	10,401	98	Paved park	ing, HSG C		
	17,617	88	Weighted Average			
	7,216		40.96% Pei			
	10,401		59.04% Imp	pervious Are	ea	
Tc	Length	Slope	,	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
6.0					Direct Entry, 6' (MIN.)	

## Summary for Subcatchment P1c: PROPOSED

Runoff = 0.26 cfs @ 12.08 hrs, Volume= 902 cf, Depth= 4.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

 Area (sf)	CN	Description		
2,307	98	Paved parking, HSG C		
 2,307		100.00% Impervious Area		

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entr	y, 6' (MIN.)		
	Summary for Subcatchment P1d: PROPOSED							
Runoff	=	2.51 cfs	s@ 12.3	8 hrs, Volu	ime=	13,129 cf, De	epth= 2.3	31"
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"							
Α	rea (sf)	CN D	escription					
	10 205	71 >	750/ Croo	a aquar Ca				

_	<u> </u>	iea (SI)		Jeschplion					
		49,295	74 >	>75% Grass cover, Good, HSG C					
		2,363	98 l	Jnconnecte	ed pavemer	nt, HSG C			
		15,500	70 V	Voods, Go	od, HSG C				
_		1,088	98 l	Jnconnecte	ed roofs, HS	SG C			
		68,246	74 V	Veighted A	verage				
		64,795	ç	94.94% Per	vious Area				
		3,451	5	5.06% Impe	ervious Are	а			
		3,451	1	00.00% Ui	nconnected	1			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	12.3	50	0.0200	0.07		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 3.21"			
	14.3	570	0.0090	0.66		Shallow Concentrated Flow,			
_						Short Grass Pasture Kv= 7.0 fps			
	26.6	620	Total						

# Summary for Subcatchment P1e: PROPOSED

0.94 cfs @ 12.24 hrs, Volume= Runoff =

4,115 cf, Depth= 2.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

Area (sf)	CN	Adj	Description
16,470	74		>75% Grass cover, Good, HSG C
700	98		Unconnected pavement, HSG C
3,133	70		Woods, Good, HSG C
1,088	98		Unconnected roofs, HSG C
21,391	75	74	Weighted Average, UI Adjusted
19,603			91.64% Pervious Area
1,788			8.36% Impervious Area
1,788			100.00% Unconnected

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.2	50	0.0140	0.06		Sheet Flow,
3.3	170	0.0150	0.86		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
17.5	220	Total			
	Summary for Subcatchment P1f: PROPOSED				
Runoff	=	2.49 cf	s@ 12.1	4 hrs, Volu	Ime= 8,914 cf, Depth= 2.48"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr  10-yr Rainfall=4.93"				ted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs	
A	rea (sf)	CN A	Adj Desc	cription	
	35,159	74			ver, Good, HSG C
	4,913	98			avement, HSG C
	2,008 1,088	98 98			oofs, HSG C oofs, HSG C
	43,168				age, UI Adjusted
	35,159	10		5% Perviou	is Area
	8,009			5% Impervi	
	8,009			00% Uncor	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.3	50	0.0400	0.20	· _ · / ·	Sheet Flow,
6.0	250	0.0100	0.70		Grass: Short n= 0.150 P2= 3.21" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
10.3	300	Total			
		S	ummary	for Subc	catchment P1g: PROPOSED
Runoff	=	1.92 cf	s@ 12.2	6 hrs, Volu	ume= 8,586 cf, Depth= 2.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

Area (sf)	CN	Adj	Description
26,694	74		>75% Grass cover, Good, HSG C
8,603	98		Unconnected pavement, HSG C
2,788	70		Woods, Good, HSG C
1,088	98		Unconnected roofs, HSG C
1,004	98		Unconnected roofs, HSG C
40,177	80	77	Weighted Average, UI Adjusted
29,482			73.38% Pervious Area
10,695			26.62% Impervious Area
10,695			100.00% Unconnected

Prepare	d by Grif	ffin Engir		roup, LLC	Type III 24-hr 10-yr Rainfall=4.93"Printed 1/3/2023O Software Solutions LLCPage 16
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.2	50	0.0100	0.05		Sheet Flow,
2.5	200	0.0350	1.31		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
18.7	250	Total			· · · · · · · · · · · · · · · · · · ·
	Summary for Subcatchment P1h: PROPOSED				
Runoff	=	4.64 cf	s@ 12.2	9 hrs, Volu	me= 21,886 cf, Depth= 2.14"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr  10-yr Rainfall=4.93"				ted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs	
A	rea (sf)	CN D	escription		
	47,534				ood, HSG C
	73,953 1,004			od, HSG C ed roofs, HS	
1	22,491		Veighted A	,	
	21,487			vious Area	
	1,004	0	.82% Impe	ervious Area	a
	1,004	1	00.00% U	nconnected	l
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Decemption
16.2	50	0.0100	0.05	· · ·	Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.21"
3.7	220	0.0200	0.99		Shallow Concentrated Flow,
0.7	66	0.1000	1.58		Short Grass Pasture Kv= 7.0 fps
0.7	00	0.1000	1.00		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.6	336	Total			

# Summary for Subcatchment P2a: PROPOSED

Runoff = 0.81 cfs @ 12.09 hrs, Volume= 2,524 cf, Depth= 2.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=4.93"

Area (sf)	CN	Description
7,205	74	>75% Grass cover, Good, HSG C
3,154	98	Unconnected pavement, HSG C
10,359	81	Weighted Average
7,205		69.55% Pervious Area
3,154		30.45% Impervious Area
3,154		100.00% Unconnected

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Tc Length Slope Veloc (min) (feet) (ft/ft) (ft/se				
6.0	Direct Entry, 6' (MIN.)			
Su	mmary for Pond CB1&2: CB1 & 2			
Inflow         =         0.26 cfs @         1           Outflow         =         0.26 cfs @         1           Primary         =         0.26 cfs @         1	00.00% Impervious, Inflow Depth = 4.69" for 10-yr event         2.08 hrs, Volume=       902 cf         2.08 hrs, Volume=       902 cf, Atten= 0%, Lag= 0.0 min         2.08 hrs, Volume=       902 cf         2.08 hrs, Volume=       902 cf         0.00 hrs, Volume=       0 cf			
Routing by Dyn-Stor-Ind method, Peak Elev= 53.74' @ 12.34 hrs Flood Elev= 55.90'				
0	Outlet Devices			
#1 Primary 53.40' #2 Secondary 55.90'	<b>10.0"</b> Round Culvert X 2.00 L= 5.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 53.40' / 53.20' S= 0.0400 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.55 sf <b>2.0' long x 2.0' breadth Broad-Crested Rectangular Weir X 2.00</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32			
Primary OutFlow Max=0.25 cfs @ 12.08 hrs HW=53.61' TW=53.52' (Dynamic Tailwater) ▲ 1=Culvert (Outlet Controls 0.25 cfs @ 1.75 fps)				
Secondary OutFlow Max=0.00 c 2=Broad-Crested Rectangula	s @ 0.00 hrs HW=53.40' TW=49.00' (Dynamic Tailwater) <b>r Weir</b> ( Controls 0.00 cfs)			
S	Summary for Pond DMH1: DMH1			

Inflow Area	a =	2,307 sf,100.00% Impervious, Inflow Depth = 4.69" for 10-yr event
Inflow	=	0.26 cfs @ 12.08 hrs, Volume= 902 cf
Outflow	=	0.26 cfs @ 12.08 hrs, Volume= 902 cf, Atten= 0%, Lag= 0.0 min
Primary	=	0.26 cfs @ 12.08 hrs, Volume= 902 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 53.73' @ 12.33 hrs Flood Elev= 56.20'

Device I	Routing	Invert	Outlet Devices
	Primary	53.20'	<b>12.0" Round Culvert</b> L= 150.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 53.20' / 52.30' S= 0.0060 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

Primary OutFlow Max=0.26 cfs @ 12.08 hrs HW=53.52' TW=53.10' (Dynamic Tailwater) ↓ 1=Culvert (Outlet Controls 0.26 cfs @ 1.76 fps)

## Summary for Pond DMH2: DMH2

Inflow Area	a =	91,944 sf, 8.21% Impervious, Inflow Depth =	2.37" for 10-yr event
Inflow	=	3.40 cfs @ 12.33 hrs, Volume= 18,147 cf	
Outflow	=	3.40 cfs @ 12.33 hrs, Volume= 18,147 cf,	, Atten= 0%, Lag= 0.0 min
Primary	=	3.40 cfs @ 12.33 hrs, Volume= 18,147 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 53.73' @ 12.33 hrs Flood Elev= 56.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	52.30'	12.0" Round Culvert
			L= 44.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 52.30' / 52.00' S= 0.0068 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

Primary OutFlow Max=3.40 cfs @ 12.33 hrs HW=53.73' TW=52.09' (Dynamic Tailwater) -1=Culvert (Barrel Controls 3.40 cfs @ 4.33 fps)

## Summary for Pond DMH3: DMH3

Inflow Area =	60,785 sf, 30.29% Impervious,	Inflow Depth = 2.80" for 10-yr event
Inflow =	3.95 cfs @ 12.12 hrs, Volume=	14,203 cf
Outflow =	3.95 cfs @ 12.12 hrs, Volume=	14,203 cf, Atten= 0%, Lag= 0.0 min
Primary =	3.95 cfs @ 12.12 hrs, Volume=	14,203 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 54.40' @ 12.12 hrs Flood Elev= 55.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	52.50'	12.0" Round Culvert
			L= 92.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 52.50' / 52.00' S= 0.0054 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

Primary OutFlow Max=3.94 cfs @ 12.12 hrs HW=54.40' TW=51.67' (Dynamic Tailwater) **1=Culvert** (Barrel Controls 3.94 cfs @ 5.02 fps)

## Summary for Pond PW1: PW #1

Inflow Area =	165,281 sf, 16.39% Impervious,	Inflow Depth = 2.54" for 10-yr event
Inflow =	6.89 cfs @ 12.13 hrs, Volume=	34,941 cf
Outflow =	4.57 cfs @ 12.48 hrs, Volume=	31,090 cf, Atten= 34%, Lag= 21.0 min
Primary =	4.57 cfs @ 12.48 hrs, Volume=	31,090 cf

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 52.17' @ 12.48 hrs Surf.Area= 5,244 sf Storage= 9,327 cf Flood Elev= 54.00' Surf.Area= 7,326 sf Storage= 20,944 cf

Plug-Flow detention time= 106.4 min calculated for 31,084 cf (89% of inflow) Center-of-Mass det. time= 54.1 min ( 891.6 - 837.5 )

Volume	Inv	vert Avail.Sto	orage Storage	e Description	
#1	50.	00' 20,9	44 cf Custor	n Stage Data (Pi	rismatic)Listed below (Recalc)
Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
50.0		3,450	0	0	
51.0		4,204	3,827	3,827	
52.0		5,015	4,610	8,437	
53.0 54.0		6,337 7,326	5,676 6,832	14,113 20,944	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	53.25'	Head (feet) 2.50 3.00 3 Coef. (Englis	0.20 0.40 0.60 .50 4.00 4.50 5	70 2.69 2.68 2.68 2.66 2.64 2.64
#2	Primary	51.00'	<b>10.0" Roun</b> L= 20.0' RC Inlet / Outlet	<b>d Culvert X 2.00</b> CP, sq.cut end pro Invert= 51.00' / 5	

Primary OutFlow Max=4.57 cfs @ 12.48 hrs HW=52.17' TW=0.00' (Dynamic Tailwater) -1=Broad-Crested Rectangular Weir (Controls 0.00 cfs) -2=Culvert (Inlet Controls 4.57 cfs @ 4.19 fps)

## Summary for Pond TR2: TR2

Inflow Area =	10,359 sf, 30.45% Impervious,	Inflow Depth = 2.92" for 10-yr event
Inflow =	0.81 cfs @ 12.09 hrs, Volume=	2,524 cf
Outflow =	0.28 cfs @ 12.39 hrs, Volume=	2,524 cf, Atten= 66%, Lag= 18.0 min
Discarded =	0.28 cfs @ 12.39 hrs, Volume=	2,524 cf
Primary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 51.06' @ 12.39 hrs Surf.Area= 1,458 sf Storage= 594 cf Flood Elev= 52.00' Surf.Area= 2,844 sf Storage= 1,957 cf

Plug-Flow detention time= 24.0 min calculated for 2,523 cf (100% of inflow) Center-of-Mass det. time= 24.0 min ( 843.7 - 819.7 )

*Type III 24-hr 10-yr Rainfall=4.93"* Printed 1/3/2023 LC Page 20

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Volume	Invert	Avail.Storage	Storage Description
#1	51.00'	705 cf	3.00'W x 114.00'L x 1.00'H Prismatoid Z=3.0
#2	49.00'	274 cf	3.00'W x 114.00'L x 2.00'H Prismatoid
			684 cf Overall x 40.0% Voids
		979 cf	x 2.00 = 1,957 cf Total Available Storage
Device	Routing	Invert Ou	tlet Devices
#1	Primary	51.90' <b>20</b> .	0' long x 6.0' breadth Broad-Crested Rectangular Weir
	-	He	ad (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
		2.5	0 3.00 3.50 4.00 4.50 5.00 5.50
		Co	ef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65
		2.6	5 2.66 2.66 2.67 2.69 2.72 2.76 2.83
#2	Discarded	49.00' <b>8.2</b>	70 in/hr Exfiltration over Surface area Phase-In= 0.01'

**Discarded OutFlow** Max=0.28 cfs @ 12.39 hrs HW=51.06' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.28 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=49.00' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

#### Summary for Link E: EXISTING

Inflow Area =	=	338,308 sf,	0.00% Impervious,	Inflow Depth = 1.98"	for 10-yr event
Inflow =	:	10.85 cfs @ '	12.36 hrs, Volume=	55,950 cf	
Primary =		10.85 cfs @ 1	12.36 hrs, Volume=	55,950 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link E1: EXISTING

Inflow Area	a =	333,614 sf,	0.00% Impervious,	Inflow Depth = 1.98"	for 10-yr event
Inflow	=	10.72 cfs @ 1	12.37 hrs, Volume=	55,173 cf	
Primary	=	10.72 cfs @ 1	12.37 hrs, Volume=	55,173 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link E2: EXISTING

 Inflow Area =
 4,694 sf,
 0.00% Impervious,
 Inflow Depth =
 1.98"
 for
 10-yr event

 Inflow =
 0.19 cfs @
 12.19 hrs,
 Volume=
 776 cf

 Primary =
 0.19 cfs @
 12.19 hrs,
 Volume=
 776 cf,
 Atten= 0%,
 Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### **Summary for Link P: PROPOSED**

 Inflow Area =
 338,308 sf, 12.40% Impervious, Inflow Depth =
 2.18" for 10-yr event

 Inflow =
 10.71 cfs @
 12.31 hrs, Volume=
 61,563 cf

 Primary =
 10.71 cfs @
 12.31 hrs, Volume=
 61,563 cf, Atten= 0%, Lag= 0.0 min

# Summary for Link P1: PROPOSED

Inflow Area	a =	327,949 sf, 11.83% Impervious, Inflow Depth = 2.25" for 10-yr event	
Inflow	=	10.71 cfs @ 12.31 hrs, Volume= 61,563 cf	
Primary	=	10.71 cfs @ 12.31 hrs, Volume= 61,563 cf, Atten= 0%, Lag= 0.0	min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

## **Summary for Link P2: PROPOSED**

Inflow Area	a =	10,359 sf,	30.45% Impervious,	Inflow Depth = 0.00"	for 10-yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	-
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

## Summary for Subcatchment E1a: EXISTING

Runoff = 30.25 cfs @ 12.33 hrs, Volume= 151,999 cf, Depth= 5.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

A	rea (sf)	CN D	escription		
3	33,614	70 V	Voods, Go	od, HSG C	
3	33,614	1	00.00% Pe	ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.2	50	0.0140	0.06		Sheet Flow,
10.5	374	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
24.7	424	Total			

### Summary for Subcatchment E2a: EXISTING

Runoff = 0.55 cfs @ 12.18 hrs, Volume= 2,139 cf, Depth= 5.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

A	rea (sf)	CN E	Description		
	4,694	70 V	Voods, Go	od, HSG C	
	4,694	1	00.00% Pe	ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.3	50	0.0200	0.07		Sheet Flow,
0.9	40	0.0200	0.71		Woods: Light underbrush n= 0.400 P2= 3.21" <b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
13.2	90	Total			

## Summary for Subcatchment P1a: PROPOSED

Runoff = 2.08 cfs @ 12.09 hrs, Volume= 6,500 cf, Depth= 6.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

 Type III 24-hr
 100-yr Rainfall=9.15"

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A	rea (sf)	CN D	Description		
	11,421	74 >	75% Gras	s cover, Go	ood, HSG C
	1,131	98 P	aved park	ing, HSG C	;
	12,552	76 V	Veighted A	verage	
	11,421	9	0.99% Per	vious Area	
	1,131	9	.01% Impe	ervious Area	а
_					
Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.2	16	0.0300	1.12		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.21"
2.7	34	0.0600	0.21		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.21"
0.1	21	0.1200	2.42		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
3.0					Direct Entry, 6' (MIN.)
6.0	71	Total			

## Summary for Subcatchment P1b: PROPOSED

Runoff = 3.43 cfs @ 12.08 hrs, Volume= 11,297 cf, Depth= 7.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

A	rea (sf)	CN	Description				
	7,216	74	>75% Gras	s cover, Go	bod, HSG C		
	10,401	98	Paved parking, HSG C				
	17,617	88	Weighted A	verage			
	7,216		40.96% Per	vious Area			
	10,401	:	59.04% Imp	pervious Are	ea		
Тс	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.0					Direct Entry, 6' (MIN.)		

## Summary for Subcatchment P1c: PROPOSED

Runoff = 0.48 cfs @ 12.08 hrs, Volume= 1,713 cf, Depth= 8.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

 Area (sf)	CN	Description
2,307	98	Paved parking, HSG C
2,307		100.00% Impervious Area

	ompanie d by Griff			<b>st</b> roup, LLC		Type III 24-hr	<i>100-yr Rainfall=9.15"</i> Printed 1/3/2023	
HydroCA	D® 10.00-2	25 s/n 013	316 © 201	9 HydroCAD	) Software Solut	tions LLC	Page 24	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry	, 6' (MIN.)		
	Summary for Subcatchment P1d: PROPOSED							
Runoff	=	6.50 cfs	s@ 12.3	6 hrs, Volu	ime= 3	33,929 cf, Depth= 5	5.97"	
Dunaff		00 m oth			tad CNL Times	Creen- 0.00 40.00 h		

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

	А	rea (sf)	CN I	Description		
		49,295	74 :	>75% Gras	s cover, Go	ood, HSG C
		2,363	98 I	Jnconnecte	ed pavemer	nt, HSG C
		15,500	70	Noods, Go	od, HSG C	
		1,088	98	Jnconnecte	ed roofs, HS	SG C
		68,246	74 \	Neighted A	verage	
		64,795	ę	94.94% Per	vious Area	
		3,451	Į	5.06% Impe	ervious Area	a
		3,451		100.00% Üi	nconnected	1
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	12.3	50	0.0200	0.07		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.21"
	14.3	570	0.0090	0.66		Shallow Concentrated Flow,
_						Short Grass Pasture Kv= 7.0 fps
	26.6	620	Total			

# Summary for Subcatchment P1e: PROPOSED

Runoff = 2.44 cfs @ 12.23 hrs, Volume=

2.23 hrs, Volume= 10,635 cf, Depth= 5.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

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IIJUIUCA		25 3/1101	510 @ 201	STIJUIOCAL	P contware conditions ELC Fage 25
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.2	50	0.0140	0.06	\$ <b>4</b>	Sheet Flow,
3.3	170	0.0150	0.86		Woods: Light underbrush n= 0.400 P2= 3.21" Shallow Concentrated Flow,
0.0		0.0100	0.00		Short Grass Pasture Kv= 7.0 fps
17.5	220	Total			
		ç	Summary	for Sub	catchment P1f: PROPOSED
			Janniary		
Runoff	=	6.19 cf	s@ 12.1	4 hrs, Volu	ume= 22,356 cf, Depth= 6.21"
			nod, UH=S fall=9.15"	CS, Weigh	nted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs
A	rea (sf)	CN A	Adj Desc	ription	
	35,159	74	>75%	6 Grass co	over, Good, HSG C
	4,913	98	Unco	onnected pa	avement, HSG C
	2,008	98			pofs, HSG C
	1,088	98	Unco	onnected ro	pofs, HSG C
	43,168	78	76 Weid	hted Avera	age, UI Adjusted
	35,159			5% Perviou	
	8,009		18.5	5% Impervi	ious Area
	8,009			00% Uncor	
Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
4.3	50	0.0400	0.20		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.21"
6.0	250	0.0100	0.70		Shallow Concentrated Flow,
10.3	300	Total			Short Grass Pasture Kv= 7.0 fps
10.0	000				
		<b>•</b>		far Cuba	established Dday DDODOCED

# Summary for Subcatchment P1g: PROPOSED

Runoff = 4.71 cfs @ 12.24 hrs, Volume= 21,223 cf, Depth= 6.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

Area (sf)	CN	Adj	Description
26,694	74		>75% Grass cover, Good, HSG C
8,603	98		Unconnected pavement, HSG C
2,788	70		Woods, Good, HSG C
1,088	98		Unconnected roofs, HSG C
1,004	98		Unconnected roofs, HSG C
40,177	80	77	Weighted Average, UI Adjusted
29,482			73.38% Pervious Area
10,695			26.62% Impervious Area
10,695			100.00% Unconnected

Tc         Length (feet)         Slope Velocity (ff/sec)         Description (cfs)           16.2         50         0.0100         0.05         Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.21"           2.5         200         0.0350         1.31         Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps           18.7         250         Total         Summary for Subcatchment P1h: PROPOSED           Runoff = 12.54 cfs @ 12.29 hrs, Volume= 58,355 cf, Depth= 5.72"           Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"           Area (sf)         CN         Description           47,534         74         >75% Grass cover, Good, HSG C           73,953         70         Woods, Good, HSG C           10,04         98         Unconnected roofs, HSG C           122,491         72         Weighted Average           12,487         99.18% Pervious Area           1,004         0.82% Impervious Area           1,004         0.020% Unconnected           Tc         Length         Slope           16.2         50         0.0100         0.05           3.7         220         0.0200         0.99           Shallow Concentrated Flow, Woods: Light un	MPMCompanies-170OrchardSt Prepared by Griffin Engineering Group, LLC HydroCAD® 10.00-25 s/n 01316 © 2019 HydroCAI					Type III 24-hr 100-yr Rainfall=9.15"Printed 1/3/2023Software Solutions LLCPage 26		
2.5       200       0.0350       1.31       Woods: Light underbrush $n = 0.400$ P2= 3.21" Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps         18.7       250       Total         Summary for Subcatchment P1h: PROPOSED         Runoff       =       12.54 cfs @       12.29 hrs, Volume=       58,355 cf, Depth= 5.72"         Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr       100-yr Rainfall=9.15"         Area (sf)       CN       Description         47,534       74       >75% Grass cover, Good, HSG C         73,953       70       Woods, Good, HSG C         1,004       98       Unconnected roofs, HSG C         122,491       72       Weighted Average         121,487       99.18% Pervious Area         1,004       0.82% Impervious Area         1,004       100.00% Unconnected         Tc< Length					• • •	Description		
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	16.2	50	0.0100	0.05				
Summary for Subcatchment P1h: PROPOSEDRunoff=12.54 cfs @12.29 hrs, Volume=58,355 cf, Depth= 5.72"Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr100-yr Rainfall=9.15"Area (sf)CNDescription47,53474>75% Grass cover, Good, HSG C 73,953701,00498Unconnected roofs, HSG C1,00498Unconnected roofs, HSG C122,49172Weighted Average 121,487121,48799.18% Pervious Area 1,004100.00% UnconnectedTcLengthSlopeVelocityCapacityDescription (ft/ft)(ft/sec)16.2500.01000.05Sheet Flow, Woods: Light underbrush n= 0.4003.72200.02000.99Shallow Concentrated Flow, Short Grass Pasture0.7660.10001.58Shallow Concentrated Flow,	2.5	200	0.0350	1.31		Shallow Concentrated Flow,		
Runoff       =       12.54 cfs @       12.29 hrs, Volume=       58,355 cf, Depth= 5.72"         Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs         Type III 24-hr       100-yr Rainfall=9.15"         Area (sf)       CN       Description         47,534       74       >75% Grass cover, Good, HSG C         73,953       70       Woods, Good, HSG C         1,004       98       Unconnected roofs, HSG C         122,491       72       Weighted Average         121,487       99.18% Pervious Area         1,004       0.82% Impervious Area         1,004       100.00% Unconnected         Tc       Length       Slope       Velocity       Capacity       Description         (min)       (feet)       (ft/ft)       (ft/sec)       (cfs)         16.2       50       0.0100       0.05       Sheet Flow,         Woods: Light underbrush n= 0.400 P2= 3.21"       Shallow Concentrated Flow,       Short Grass Pasture       Kv= 7.0 fps         0.7       66       0.1000       1.58       Shallow Concentrated Flow,       Short Grass Pasture	18.7	250	Total					
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrsType III 24-hr 100-yr Rainfall=9.15"Area (sf)CNDescription47,53474>75% Grass cover, Good, HSG C73,95370Woods, Good, HSG C1,00498Unconnected roofs, HSG C122,49172Weighted Average121,48799.18% Pervious Area1,0040.82% Impervious Area1,004100.00% UnconnectedTcLengthGreet(ft/ft)(min)(feet)(ft/ft)(ft/sec)(cfs)Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.21"3.72200.02000.99Shallow Concentrated Flow, Short Grass Pasture0.7660.10001.58Shallow Concentrated Flow, Short Grass Pasture		Summary for Subcatchment P1h: PROPOSED						
Type III 24-hr 100-yr Rainfall=9.15"Area (sf)CNDescription47,53474>75% Grass cover, Good, HSG C73,95370Woods, Good, HSG C1,00498Unconnected roofs, HSG C122,49172Weighted Average121,48799.18% Pervious Area1,0040.82% Impervious Area1,004100.00% UnconnectedTcLengthGreetGft/ft)(min)(feet)(ft/ft)(ft/sec)(cfs)16.2500.01000.05Sheet Flow, Woods: Light underbrush3.72200.02000.99Shallow Concentrated Flow, Short Grass PastureKv= 7.0 fps0.7660.10001.58Shallow Concentrated Flow, Shallow Concentrated Flow,	Runoff	=	12.54 cfs	s@ 12.2	9 hrs, Volu	me= 58,355 cf, Depth= 5.72"		
47,534       74       >75% Grass cover, Good, HSG C         73,953       70       Woods, Good, HSG C         1,004       98       Unconnected roofs, HSG C         122,491       72       Weighted Average         121,487       99.18% Pervious Area         1,004       0.82% Impervious Area         1,004       0.82% Impervious Area         1,004       100.00% Unconnected         Tc       Length         Slope       Velocity       Capacity         Description       (ft/ft)         (min)       (feet)       (ft/sec)         16.2       50       0.0100       0.05         Sheet Flow,       Woods: Light underbrush n= 0.400       P2= 3.21"         3.7       220       0.0200       0.99       Shallow Concentrated Flow, Short Grass Pasture         0.7       66       0.1000       1.58       Shallow Concentrated Flow,	Type III 2	24-hr 100	0-yr Rainf	all=9.15"		ted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs		
1,004         98         Unconnected roofs, HSG C           122,491         72         Weighted Average           121,487         99.18% Pervious Area           1,004         0.82% Impervious Area           1,004         0.82% Impervious Area           1,004         100.00% Unconnected           Tc         Length         Slope         Velocity         Capacity           (min)         (feet)         (ft/ft)         (ft/sec)         (cfs)           16.2         50         0.0100         0.05         Sheet Flow,           Woods: Light underbrush         n= 0.400         P2= 3.21"           3.7         220         0.0200         0.99         Shallow Concentrated Flow, Short Grass Pasture           0.7         66         0.1000         1.58         Shallow Concentrated Flow,						ood, HSG C		
122,491       72       Weighted Average         121,487       99.18% Pervious Area         1,004       0.82% Impervious Area         1,004       100.00% Unconnected         Tc       Length       Slope       Velocity       Capacity         (min)       (feet)       (ft/ft)       (ft/sec)       (cfs)         16.2       50       0.0100       0.05       Sheet Flow,         3.7       220       0.0200       0.99       Shallow Concentrated Flow, Short Grass Pasture       Kv= 7.0 fps         0.7       66       0.1000       1.58       Shallow Concentrated Flow,								
121,487       99.18% Pervious Area         1,004       0.82% Impervious Area         1,004       100.00% Unconnected         Tc       Length       Slope       Velocity       Capacity         (min)       (feet)       (ft/ft)       Capacity       Description         16.2       50       0.0100       0.05       Sheet Flow,         3.7       220       0.0200       0.99       Shallow Concentrated Flow, Short Grass Pasture         0.7       66       0.1000       1.58       Shallow Concentrated Flow,					,	SG C		
1,0040.82% Impervious Area1,004100.00% UnconnectedTcLengthSlopeVelocityCapacity (ft/ft)Description(min)(feet)(ft/ft)(ft/sec)Description16.2500.01000.05Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.21"3.72200.02000.99Shallow Concentrated Flow, Short Grass Pasture0.7660.10001.58Shallow Concentrated Flow, Shallow Concentrated Flow, Shallow Concentrated Flow,								
1,004100.00% UnconnectedTcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)Description16.2500.01000.05Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.21"3.72200.02000.99Shallow Concentrated Flow, Short Grass Pasture0.7660.10001.58Shallow Concentrated Flow, Shallow Concentrated Flow,	I		-					
(min)         (feet)         (ft/ft)         (ft/sec)         (cfs)           16.2         50         0.0100         0.05         Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.21"           3.7         220         0.0200         0.99         Shallow Concentrated Flow, Short Grass Pasture         Kv= 7.0 fps           0.7         66         0.1000         1.58         Shallow Concentrated Flow,								
16.2         50         0.0100         0.05         Sheet Flow, Woods: Light underbrush         n= 0.400         P2= 3.21"           3.7         220         0.0200         0.99         Shallow Concentrated Flow, Short Grass Pasture         Kv= 7.0 fps           0.7         66         0.1000         1.58         Shallow Concentrated Flow, Short Grass Pasture         Kv= 7.0 fps		Length				Description		
3.7       220       0.0200       0.99       Shallow Concentrated Flow, Short Grass Pasture       Kv= 7.0 fps         0.7       66       0.1000       1.58       Shallow Concentrated Flow,	i				· · · · ·	Sheet Flow,		
0.7 66 0.1000 1.58 Shallow Concentrated Flow,	3.7	220	0.0200	0.99		Shallow Concentrated Flow,		
	0.7	66	0.1000	1.58		Shallow Concentrated Flow,		

20.6 336 Total

## Summary for Subcatchment P2a: PROPOSED

Runoff = 1.85 cfs @ 12.09 hrs, Volume= 5,900 cf, Depth= 6.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=9.15"

Area (sf)	CN	Description
7,205	74	>75% Grass cover, Good, HSG C
3,154	98	Unconnected pavement, HSG C
10,359	81	Weighted Average
7,205		69.55% Pervious Area
3,154		30.45% Impervious Area
3,154		100.00% Unconnected

MPMCompanies-170OrchardSt Prepared by Griffin Engineering Group, LLC HydroCAD® 10.00-25 s/n 01316 © 2019 HydroCAD									
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)					
6.0					Direct Entry, 6' (MIN.)				
	Summary for Pond CB1&2: CB1 & 2								
Inflow Outflow Primary	Inflow Area =       2,307 sf,100.00% Impervious, Inflow Depth = 8.91" for 100-yr event         Inflow =       0.48 cfs @       12.08 hrs, Volume=       1,713 cf         Outflow =       0.48 cfs @       12.08 hrs, Volume=       1,713 cf, Atten= 0%, Lag= 0.0 min         Primary =       0.48 cfs @       12.08 hrs, Volume=       1,583 cf         Secondary =       0.32 cfs @       12.17 hrs, Volume=       256 cf								
Peak Ele	Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 55.99' @ 12.18 hrs Flood Elev= 55.90'								
Device	Routing		Invert C	outlet Device	ces				
#1       Primary       53.40'       10.0"       Round         L= 5.0'       RCP         Inlet / Outlet I       n= 0.011       Cor         #2       Secondary       55.90'       2.0'       long x 2         Head (feet)       0       2.50       3.00       3.40'					nd Culvert X 2.00         CP, sq.cut end projecting, Ke= 0.500         t Invert= 53.40' / 53.20' S= 0.0400 '/' Cc= 0.900         concrete pipe, straight & clean, Flow Area= 0.55 sf         2.0' breadth Broad-Crested Rectangular Weir X 2.00         0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00         3.50         ish) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88				
			2	.85 3.07 3	3.20 3.32				
	<b>OutFlow</b> Ilvert(Co			2.08 hrs H	HW=54.49' TW=54.61' (Dynamic Tailwater)				
0			0.00.5	~ 40 47 1					

Secondary OutFlow Max=0.00 cfs @ 12.17 hrs HW=54.27' TW=51.71' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

## Summary for Pond DMH1: DMH1

Inflow Area =	2,307 sf,100.00% Impervious,	Inflow Depth = 8.23" for 100-yr event
Inflow =	0.48 cfs @ 12.08 hrs, Volume=	1,583 cf
Outflow =	0.48 cfs @ 12.08 hrs, Volume=	1,583 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.48 cfs @ 12.08 hrs, Volume=	1,583 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 58.77' @ 12.33 hrs Flood Elev= 56.20'

Device Routing Invert Outlet Devices	
#1 Primary 53.20' <b>12.0'' Round Culvert</b> L= 150.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 53.20' / 52.30' S= 0.0060 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf	

Primary OutFlow Max=0.48 cfs @ 12.08 hrs HW=54.61' TW=54.58' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.48 cfs @ 0.61 fps)

## Summary for Pond DMH2: DMH2

Inflow Area	=	91,944 sf,	8.21% Impervious,	Inflow Depth = 6.02"	for 100-yr event
Inflow =	=	8.78 cfs @	12.33 hrs, Volume=	46,147 cf	
Outflow =	=	8.78 cfs @	12.33 hrs, Volume=	46,147 cf, Atte	n= 0%, Lag= 0.0 min
Primary =	=	8.78 cfs @	12.33 hrs, Volume=	46,147 cf	-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 58.98' @ 12.33 hrs Flood Elev= 56.50'

Device	Routing	Invert	Outlet Devices
	Primary	52.30'	<b>12.0" Round Culvert</b> L= 44.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 52.30' / 52.00' S= 0.0068 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

Primary OutFlow Max=8.78 cfs @ 12.33 hrs HW=58.98' TW=53.60' (Dynamic Tailwater) -1=Culvert (Inlet Controls 8.78 cfs @ 11.17 fps)

#### Summary for Pond DMH3: DMH3

Inflow Area =	60,785 sf, 30.29% Impervious,	Inflow Depth = 6.64" for 100-yr event
Inflow =	9.20 cfs @ 12.12 hrs, Volume=	33,653 cf
Outflow =	9.20 cfs @ 12.12 hrs, Volume=	33,653 cf, Atten= 0%, Lag= 0.0 min
Primary =	9.20 cfs @ 12.12 hrs, Volume=	33,653 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 60.60' @ 12.12 hrs Flood Elev= 55.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	52.50'	12.0" Round Culvert
			L= 92.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 52.50' / 52.00' S= 0.0054 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

## Summary for Pond PW1: PW #1

Inflow Area =	165,281 sf, 16.39% Impervious,	Inflow Depth = 6.27" for 100-yr event
Inflow =	17.01 cfs @ 12.13 hrs, Volume=	86,300 cf
Outflow =	13.27 cfs @ 12.38 hrs, Volume=	82,449 cf, Atten= 22%, Lag= 14.7 min
Primary =	13.27 cfs @ 12.38 hrs, Volume=	82,449 cf

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 53.61' @ 12.38 hrs Surf.Area= 6,942 sf Storage= 18,175 cf Flood Elev= 54.00' Surf.Area= 7,326 sf Storage= 20,944 cf

Plug-Flow detention time= 64.8 min calculated for 82,449 cf (96% of inflow) Center-of-Mass det. time= 39.5 min ( 853.2 - 813.7 )

Volume	Inv	ert Avail.Sto	rage Storage	age Storage Description				
#1	50.	00' 20,94	44 cf Custon	n Stage Data (Pr	<b>ismatic)</b> Listed below (Recalc)			
Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
50.0		3,450	0	0				
51.0		4,204	3,827	3,827				
52.0		5,015	4,610	8,437				
53.0		6,337	5,676	14,113				
54.0	00	7,326	6,832	20,944				
Device	Routing	Invert	Outlet Device	S				
#1	Primary	53.25'			oad-Crested Rectangular Weir			
			2.50 3.00 <sup>^</sup> 3. Coef. (Englisl 2.64 2.65 2.	50 4.00 4.50 5 n) 2.43 2.54 2. 65 2.66 2.66 2	70 2.69 2.68 2.68 2.66 2.64 2.64			
#2	Primary	51.00'	L= 20.0' RC Inlet / Outlet I	nvert= 51.00' / 5	ojecting, Ke= 0.500 0.50' S= 0.0250 '/' Cc= 0.900 or, Flow Area= 0.55 sf			

Primary OutFlow Max=13.26 cfs @ 12.38 hrs HW=53.61' TW=0.00' (Dynamic Tailwater) -1=Broad-Crested Rectangular Weir (Weir Controls 5.48 cfs @ 1.52 fps) -2=Culvert (Inlet Controls 7.78 cfs @ 7.13 fps)

#### Summary for Pond TR2: TR2

Inflow Area =	10,359 sf, 30.45% Impervious,	Inflow Depth = 7.13" for 100-yr event
Inflow =	1.85 cfs @ 12.09 hrs, Volume=	6,155 cf
Outflow =	0.68 cfs @ 12.42 hrs, Volume=	6,155 cf, Atten= 63%, Lag= 19.9 min
Discarded =	0.52 cfs @ 12.42 hrs, Volume=	6,077 cf
Primary =	0.16 cfs @ 12.42 hrs, Volume=	78 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 51.92' @ 12.42 hrs Surf.Area= 2,725 sf Storage= 1,795 cf Flood Elev= 52.00' Surf.Area= 2,844 sf Storage= 1,957 cf

Plug-Flow detention time= 32.6 min calculated for 6,155 cf (100% of inflow) Center-of-Mass det. time= 32.6 min ( 825.9 - 793.3 )

 Type III 24-hr
 100-yr Rainfall=9.15"

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Volume	Invert	Avail.Storage	e Storage Description
#1	51.00'	705 c	of 3.00'W x 114.00'L x 1.00'H Prismatoid Z=3.0
#2	49.00'	274 c	of 3.00'W x 114.00'L x 2.00'H Prismatoid
			684 cf Overall x 40.0% Voids
		979 c	of x 2.00 = 1,957 cf Total Available Storage
Device	Routing	Invert O	utlet Devices
#1	Primary	51.90' <b>20</b>	0.0' long x 6.0' breadth Broad-Crested Rectangular Weir
	-	H	ead (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
		2.	50 3.00 3.50 4.00 4.50 5.00 5.50
		C	pef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65
		2.	65 2.66 2.66 2.67 2.69 2.72 2.76 2.83
#2	Discarded	49.00' <b>8.</b>	270 in/hr Exfiltration over Surface area Phase-In= 0.01'

**Discarded OutFlow** Max=0.52 cfs @ 12.42 hrs HW=51.92' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.52 cfs)

Primary OutFlow Max=0.16 cfs @ 12.42 hrs HW=51.92' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 0.16 cfs @ 0.36 fps)

### Summary for Link E: EXISTING

Inflow Area	a =	338,308 sf,	0.00% Impervious,	Inflow Depth = 5.47"	for 100-yr event
Inflow	=	30.63 cfs @ 1	2.33 hrs, Volume=	154,137 cf	•
Primary	=	30.63 cfs @ 1	2.33 hrs, Volume=	154,137 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link E1: EXISTING

Inflow Area	a =	333,614 sf,	0.00% Impervious,	Inflow Depth = 5.47"	for 100-yr event
Inflow	=	30.25 cfs @ 1	12.33 hrs, Volume=	151,999 cf	
Primary	=	30.25 cfs @ 1	12.33 hrs, Volume=	151,999 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link E2: EXISTING

 Inflow Area =
 4,694 sf,
 0.00% Impervious,
 Inflow Depth =
 5.47"
 for
 100-yr event

 Inflow =
 0.55 cfs @
 12.18 hrs,
 Volume=
 2,139 cf

 Primary =
 0.55 cfs @
 12.18 hrs,
 Volume=
 2,139 cf,
 Atten= 0%,
 Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Summary for Link P: PROPOSED

 Inflow Area =
 338,308 sf, 12.40% Impervious, Inflow Depth =
 5.75" for 100-yr event

 Inflow =
 29.38 cfs @
 12.32 hrs, Volume=
 162,104 cf

 Primary =
 29.38 cfs @
 12.32 hrs, Volume=
 162,104 cf, Atten= 0%, Lag= 0.0 min

# Summary for Link P1: PROPOSED

Inflow Area	a =	327,949 sf,	11.83% Impervious,	Inflow Depth = 5.93"	for 100-yr event
Inflow	=	29.38 cfs @	12.32 hrs, Volume=	162,026 cf	•
Primary	=	29.38 cfs @	12.32 hrs, Volume=	162,026 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

## **Summary for Link P2: PROPOSED**

Inflow Area	a =	10,359 sf, 30.45% Impervious, Inflow Depth = 0.09" for 100-y	event
Inflow	=	0.16 cfs @ 12.42 hrs, Volume= 78 cf	
Primary	=	0.16 cfs @ 12.42 hrs, Volume= 78 cf, Atten= 0%, Lag	j= 0.0 min